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# Effect of activated $\text{NH}_3$ on $\text{SO}_2$ removal by pulse corona discharge plasma in flue gas

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**Abstract:**  $\text{NH}_3$ -activated electrode is placed in front of the electrode system of pulse corona discharge plasma. There are nozzles on the electrode. Positive DC high-voltage is applied on the nozzle-plate gap.  $\text{NH}_3$  is injected into the reactor through nozzles, at the same time, activated and treated. These nozzles were proposed in order to make the additional gas pass through corona discharge regions near the tip of nozzles and increase the amount of radicals. The aim is to improve the De- $\text{SO}_2$  efficiency by pulse discharge plasma in flue gas. The following topics are investigated and discussed in the paper: De- $\text{SO}_2$  effect of single  $\text{NH}_3$ -activated electrode, De- $\text{SO}_2$  effect of activated  $\text{NH}_3$ , the relationship between stoichiometric ratio of  $\text{NH}_3$  to  $\text{SO}_2$  and De- $\text{SO}_2$  effect of activated  $\text{NH}_3$ , mechanism of activated  $\text{NH}_3$  De- $\text{SO}_2$  effect. The experimental result indicates that the De- $\text{SO}_2$  efficiency can be increased 5%—10% by activated  $\text{NH}_3$  on the original base of De- $\text{SO}_2$  efficiency.

**Key words:** activated  $\text{NH}_3$ ; De- $\text{SO}_2$ ; pulse discharge

## Introduction

Now  $\text{SO}_2$  is the one of main gas pollutants and the main cause of acid rain problem.  $\text{SO}_2$  removal by pulse corona discharge is a new De- $\text{SO}_2$  technique developed during last ten years (Masuda, 1993; Mizuno, 1986; Dinelli, 1990).  $\text{SO}_2$  in flue gas is oxidized by activated radical (such as OH,  $\text{HO}_2$ ,  $\text{NH}_2$ , O) which are generated by corona discharge. With  $\text{NH}_3$  being injected into the reactor, the final product is ammonium sulfate, which is well known as fertilizer (Wu, 1998). For the oxidized efficiency, the main influence factor is the yield of radical. Recent studies have appeared with investigation on improving the yield of radical (Chang, 1991).

$\text{NH}_3$  has two effects in De- $\text{SO}_2$  process. First,  $\text{NH}_3$  acts as additional gas and reacts with  $\text{SO}_2$  ammonium sulfate; second, under the condition of corona discharge,  $\text{NH}_3$  provides strong oxidized radical, such as NH,  $\text{NH}_2$  and so on. However, the stoichiometric ratio of  $\text{NH}_3$  to  $\text{SO}_2$  is less than or equal to 1:1, the concentration of  $\text{NH}_3$  in flue gas is very low. But the collision between high-energy electron and gas molecule is unselective, so the quantity of radical correspond to  $\text{NH}_3$  is very small. Thus, promoting the collision between  $\text{NH}_3$  molecule and high energy electron is one of the effective methods to improve De- $\text{SO}_2$  efficiency.

$\text{NH}_3$  is injected into the reactor through nozzles and pass through corona discharge. By this method, the yield of activated radical corresponds to  $\text{NH}_3$  and the oxidization of  $\text{SO}_2$  is increased. Thus, we get the purpose of improving De- $\text{SO}_2$  efficiency.

## 1 Experimental configuration

The experimental configuration is shown in Fig. 1. The reactor (1) includes activated electrode system and pulse corona discharge electrode system. Activated electrode system consists of nozzle discharge electrode(2) and plate electrode(4); pulse corona discharge electrode consists of line(star-shaped) discharge electrode(3) and plate electrode(4). (5) is a positive high DC power; (6) is a rotate spark-gap pulse power. The schematic diagram of nozzle electrode (2) is shown as Fig. 2. The main body of the electrode is a pipe, 300 mm in length, outside diameter is 10 mm, inside diameter is 8 mm. Nozzle is 30 mm in length, outside diameter 2 mm, inside diameter 1 mm. The distance(D) between nozzle is 50 mm. The plate electrode (4) (500 mm × 900 mm) is

grounded. Air and  $\text{SO}_2$  mixture gases act as the simulation gas. The concentration of  $\text{SO}_2$  can be adjusted. The simulation gas is heated to  $60\text{--}80^\circ\text{C}$  and flows into the reactor. The flow rate and the volume ratio of water in flue gas are  $10\text{ m}^3\text{ h}^{-1}$  and  $0.8\%$ .

Voltage signal is detected by HP-60 high-voltage probe (Iwasu, Electric Inc., Japan), current signal by TM502A current probe (Tektronix Inc., USA). The concentration of  $\text{SO}_2$  is measured by IRA-107  $\text{SO}_2$  analyzer (Shimadzu Inc., Japan).

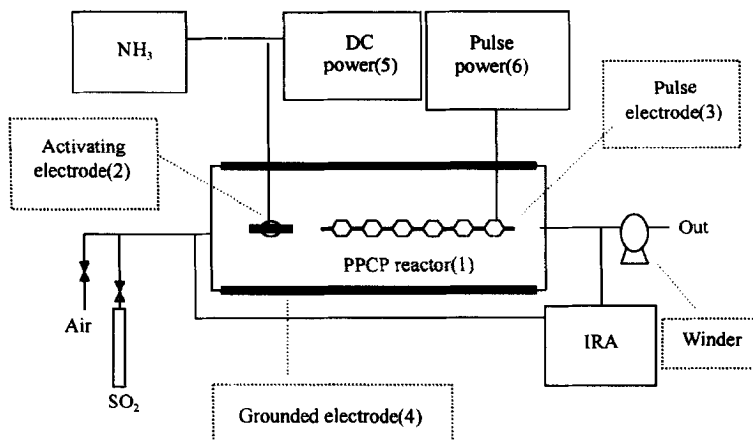


Fig.1 Experimental configuration

## 2 Discharge V-I characteristics and pulse waveform of corona discharge

Discharge V-I characteristic in activated electrode system is shown in Fig. 3. It shows that corona current increases with voltage. Thus, the energy in activated field can be calculated. The energy consumption of unit volume flue gas and  $\text{NH}_3$  also can be calculated. Typical pulse waveform of corona discharge applied on the reactor is shown in Fig. 4.

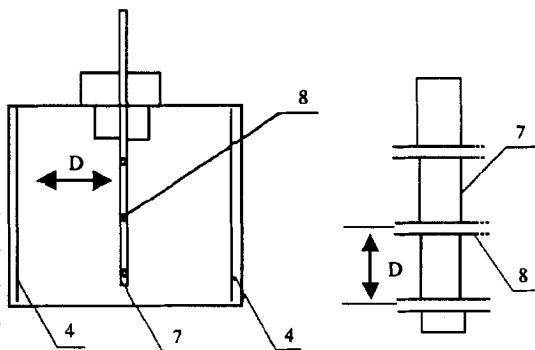


Fig.2 Structure of nozzle electrode

## 3 Experimental results and discussion

### 3.1 The effect of activated $\text{NH}_3$ for De- $\text{SO}_2$ efficiency

The stoichiometric ratio of  $\text{NH}_3$  to  $\text{SO}_2$  is  $1:1$ , and the initial density of  $\text{SO}_2$  is  $1760\text{ ppm}$ , no pulsed voltage is applied. Under the condition of activated  $\text{NH}_3$ , the relation curve of De- $\text{SO}_2$  efficiency and activated voltage is shown in Fig. 5. According to the curve, De- $\text{SO}_2$  efficiency increases with voltage. When the voltage is  $28\text{ kV}$ , the De- $\text{SO}_2$  efficiency can be increased by  $9\%$  above the original basis of thermal reaction, which is shown as the dotted line ( $\eta = 66\%$ ) in Fig. 5. The total removal rate is up to  $75\%$ . The increased removal rate due to the following reasons. The electric field intensity is reinforced because of the increased voltage applied to the  $\text{NH}_3$ -activated electrode. The collision probability between the electrons with high energy and  $\text{NH}_3$  molecule is improved. This brings about the increments of energy and the yield of activated  $\text{NH}_3$  radicals ( $\text{NH}$ ,  $\text{NH}_2$ ).

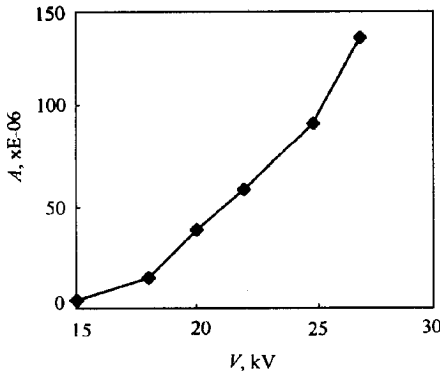


Fig. 3 V-I characteristics of corona discharge on activated electrode

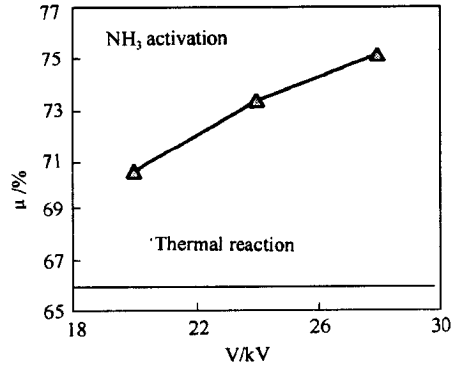


Fig. 4 Typical pulse waveform of corona discharge

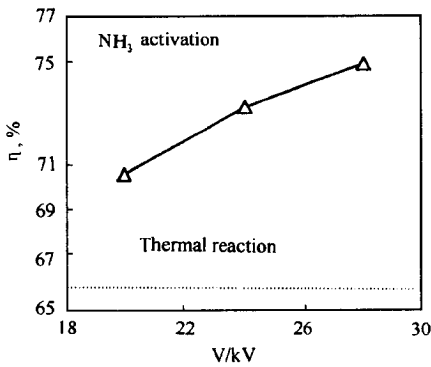


Fig. 5 Relationship between voltage of NH<sub>3</sub> activation and De-SO<sub>2</sub>

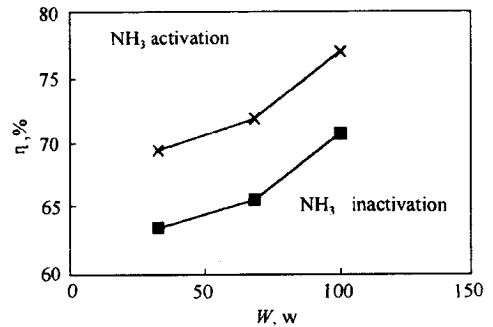


Fig. 6 Activated effect curve of De-SO<sub>2</sub> pulse discharge

### 3.2 The effect of activated NH<sub>3</sub> for SO<sub>2</sub> removal rate in the condition of pulse corona

The stoichiometric ratio of NH<sub>3</sub> to SO<sub>2</sub> is 1:1, the initial density of SO<sub>2</sub> is 1520 ppm, DC high voltage (28 kV) is applied to activate NH<sub>3</sub>. Pulse voltage is added on the line electrode. Under the conditions which NH<sub>3</sub> is activated and not, Fig. 6 shows the relationship between De-SO<sub>2</sub> efficiency of pulse corona discharge and pulse energy. According to Fig. 6, De-SO<sub>2</sub> efficiency increases with the pulse energy and under the same energy, De-SO<sub>2</sub> efficiency with activated NH<sub>3</sub> is higher apparently than that NH<sub>3</sub> is not activated. Under the experimental conditions and when activating voltage is 28 kV, De-SO<sub>2</sub> efficiency increase by 6% because of the activated NH<sub>3</sub>. There are two reasons. The first is that the pulse energy rises improves the oxidized rate from S<sup>4+</sup> to S<sup>6+</sup> in the pulse corona discharge fields; second, NH<sub>3</sub>-activated brings conditions to De-SO<sub>2</sub> by pulsed discharge in the later process (the reason of improving De-SO<sub>2</sub> efficiency with activated NH<sub>3</sub> was discussed in 3.1).

### 3.3 The influence of activated NH<sub>3</sub> quality on De-SO<sub>2</sub> efficiency

The initial density of SO<sub>2</sub> is 1520 ppm. DC voltage is 28 kV. No pulse voltage is applied to NH<sub>3</sub>-activated electrode. The stoichiometric ratio of NH<sub>3</sub> to SO<sub>2</sub> is 0.6, 0.8 and 1.0 respectively. Under the two conditions that NH<sub>3</sub> is activated (NH<sub>3</sub> is injected in NH<sub>4</sub>-activated electrode) and not (NH<sub>3</sub> is injected into front end of reactor directly). Fig. 7 shows the relationship between De-SO<sub>2</sub> efficiency and R (stoichiometric ratio). The figure indicates that the De-SO<sub>2</sub> efficiency increases with R. When R is the same, the De-SO<sub>2</sub> efficiency with activated NH<sub>3</sub> is clearly higher than that

with NH<sub>3</sub> is not activated. In the same time, the increment between the two lines is improved with R.

Under the conditions of this experiment, when R is 1.0, the improved value of De-SO<sub>2</sub> efficiency can reach 9.5% and the total De-SO<sub>2</sub> efficiency by NH<sub>3</sub> activation and thermal reaction is up to 67%. This is because R is increased, then, the quality of activated NH<sub>3</sub> is increased too. This means more radicals(NH, NH<sub>2</sub>) are generated, thus, the De-SO<sub>2</sub> efficiency is increased.

**4 Discussion on activation mechanism**

Fig. 8 shows the mechanism of NH<sub>3</sub>

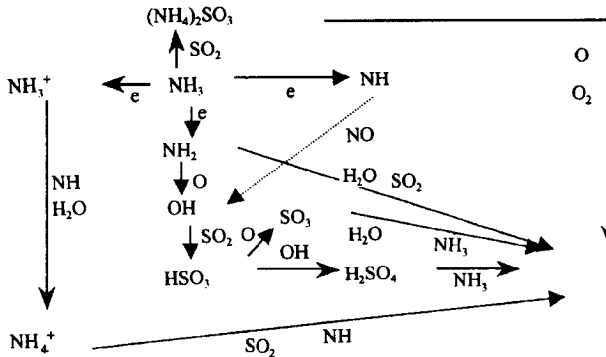


Fig.8 The mechanism of NH<sub>3</sub> activation

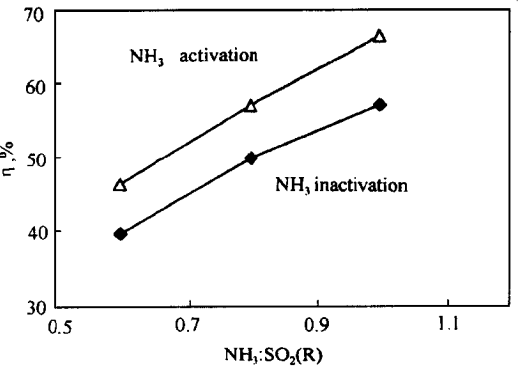


Fig.7 Curve of relationship between quality of activated NH<sub>3</sub> and De-SO<sub>2</sub> efficiency

activation. When NH<sub>3</sub> is distributed in DC electric field, the collision probability between NH<sub>3</sub> and high-energy electrons, and then, NH<sub>3</sub> is decomposed and ionized. More radicals (such as NH, NH<sub>2</sub>, NH<sub>3</sub>, OH, etc.) are produced. These radicals react with SO<sub>2</sub> molecules. Thus, SO<sub>2</sub> is transformed to no-polluted substance.

**5 Conclusion**

- (1) De-SO<sub>2</sub> efficiency by NH<sub>3</sub> activation increases with activating voltage.
- (2) NH<sub>3</sub> activation makes De-SO<sub>2</sub> efficiency increased apparently.
- (3) The improved value of De-SO<sub>2</sub> efficiency by NH<sub>3</sub>-activation effect increases with stoichiometric ratio of NH<sub>3</sub> and SO<sub>2</sub>.

(4) Under the conditions of this experiment, NH<sub>3</sub> activation effect on De-SO<sub>2</sub> efficiency is up to 5%—10%.

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